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DRAFT Characterization Analysis Report Surface Vessel Bilgewater/Oil Water Separator

Section 3.0 – CVN 68 Class: Nuclear Steam Propulsion Aircraft Carriers

SECTION 3.0 – CVN 68 CLASS

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3.0 CVN 68 CLASS

Vessels with nuclear steam propulsion refers to Aircraft Carriers. This vessel group is comprised of ten CVN 68 Nimitz Class Aircraft Carriers and one CVN 65 Class vessel. CVN 68, USS NIMITZ, was identified as the representative vessel for this vessel group. This chapter presents the physical parameters, chemical data, field data, descriptive information, and generation rates for the CVN 68 Class vessels.

For vessels with nuclear steam propulsion, water from numerous bilge wells combines with oily waste in the oily waste holding tank (OWHT) for processing by one or both of the ship's oil water separators (OWS). The bilge wells are discrete areas of the bilge that function as a critical component of the entire bilge system. They function to collect fluid until the volume reaches a level where a bilge pump can be used to transfer the liquid into the OWHT. As a result, the OWS influent is a mixture of bilgewater and oily waste from various bilge systems. Sampling was conducted aboard one of the ships in this group, USS JOHN C. STENNIS (CVN 74), in March 1998.

The primary bilge OWS system currently installed onboard CVN 68 Class vessels includes two 50-gpm gravity coalescers with a total processing rate of 100 gpm. These vessels typically process bilgewater both pierside and underway, discharging the processed effluent into the surrounding waters. The processing needs of the ship within 12 nm are generally met through the use of one 50-gpm system therefore, subsequent characterization analyses are based on a 50-gpm system processing the entire volume of bilgewater (Smith, B., 2001).

The following summarizes the general characteristics of CVN 68 Class vessels.

General Vessel Characteristics (Navy, 2001a)

Draft (ft): 40
Length at waterline (ft): 1040
Beam at water line (ft): 134
Displacement (tons): 101,196

3.1 BASELINE DISCHARGE

The baseline discharge is defined as the direct discharge of the bilgewater collected in the OWHT. This discharge is assumed to occur at the normal OWS flow rate while bypassing the OWS. It is important to note that although the term baseline discharge is used for this report, Armed Forces vessels do not discharge bilgewater from the OWHT directly overboard without treatment. This scenario is included in the Uniform National Discharge Standards (UNDS) analysis only to establish a reference point for subsequent comparisons. The baseline analysis will be based on discharging the entire volume of untreated bilgewater overboard at 50 gpm through a single OWS system discharge port.

3.1.1 Characterization Data

Sources of bilgewater aboard the CVN 68 Class vessels include liquid that drains from the interior spaces and upper decks into the bilge or lowest inner part of the vessel's hull (Navy, 2001b).

Sources of bilgewater can be found in shipboard wastestreams, such as steam condensate, boiler blowdown, drinking fountain water, and sink drainage located in various machinery spaces; leaks from tanks, pump packing glands as well as leaking piping, valves, and flanges; spills from the ship's propulsion and auxiliary systems; runoff from housekeeping (e.g. washing of deck plates or equipment); and precipitation and greenwater. The liquid phase of this fluid may be contaminated with oily constituents composed primarily of JP-5 fuel (aircraft), F-76 (emergency diesel generators), 2190TEP lube oil (main engines and auxiliary equipment), Diesel Fuel Marine (emergency diesel generators), and MIL-D-9250 lube oil (emergency diesel generators). To a lesser extent, hydraulic oil (elevators, cranes, and winches) and various grades of grease lubricants (pulleys, cables, valves, and other components) may be found in the bilgewater. Contributions to water constituents include detergents (or surfactants), corrosion products from metal surfaces, and discharges from sinks used to perform maintenance on engine room equipment. Additional potential bilge constituents include dissolved metals and metal-containing particulate matter.

3.1.1.1 Physical Parameters

The physical parameters presented in this section include values necessary for hydrodynamic modeling of the discharge, which differs from shipboard data. The characteristics of the CVN 68 baseline discharge (Table 3-1) were developed using the assumption that bilgewater is discharged overboard at the OWS design flow rate while bypassing the OWS.

Table 3-1. Discharge Characteristics for CVN 68 Baseline

| Modeling Parameters | Values |
|----------------------------------|----------|
| Option Group | Baseline |
| Vertical (ft) | 3.2 |
| Transverse (ft) | 67 |
| Length (ft) | 885 |
| Diameter (in) | 3 |
| Temperature (°C) | 25 |
| Salinity (ppt) | 8.9 |
| Flow (gpm) | 50 |
| Velocity (ft/sec) | 2.3 |
| Duration of Release Event (hr) | 16.6 |
| Time Between Release Events (hr) | 36.8 |

Vertical – Approximate distance from waterline to discharge port (+, above, -, below)

Transverse – Distance from centerline to discharge port (+, port, -, stbd)

Length – Approximate distance from forward perpendicular to discharge port

Diameter - Diameter of discharge port

ppt-parts per thousand

gpm - gallons per minute

ft/sec – feet per second

hr – hour

°C – Degree Celsius

The influent of the OWS is characterized in this report as the baseline from which a relative analysis of the marine pollution control device (MPCD) options can be performed. The parameters for the engineering and modeling recommendation summary are based on the specifications in the CVN 68 installation drawings of the OWS and a ship check.

Several parameters were identified for the discharge port on CVN 68. These parameters include: discharge port location in relation to the waterline (vertical), distance from the centerline to discharge port (transverse), approximate distance from forward perpendicular to discharge port (length), and discharge port diameter (diameter). Of those parameters, the length, transverse, and diameter parameters were obtained via CVN 68 OWS system drawing (NAVSEA Drawing No. 508-7237962), whereas the vertical modeling parameter is based on the waterline CVN 68 RCOH ship check/Configuration Drawing and OWS system drawing (Navy, 2001b). Based on full load conditions, the waterline for CVN 68 is 38.8 feet above the baseline. Additional discharge characteristics identified for modeling purposes include temperature, salinity, flow rate, discharge velocity, duration of release event, and time between release events.

The temperature of bilgewater is dependent on several factors. Bilgewater on a CVN 68 Class vessel is temporarily held in the ship's bilge or in an OWHT. Consequently, ambient air temperature inside the machinery space and the temperature of the source bilgewater can have an effect on bilgewater temperature. However, because the bilge and OWHT are separated from the water body only by the ship's hull, bilgewater is often at or near the ambient water temperature. Because bilgewater is not used as cooling or heating fluid, and there is ample opportunity for thermal equilibration (heat transfer through the metal hull), bilgewater is assumed to be at the

temperature of the receiving water. Furthermore, for modeling purposes, the ambient water temperature is assumed to be 25° C.

Unlike other parameters used for modeling purposes, sampling data from the OWS influent were used to determine the salinity value for CVN 68 baseline discharge (Navy, 1998). To facilitate obtaining a representative salinity value, an average of the sample results was used to determine one representative salinity value for the baseline discharge (the same value is used for subsequent analysis of the primary treatment MPCD; see Section 3.2.1.1).

Of the remaining discharge characteristics required for modeling flow, velocity, and duration of release event are interdependent. The exit velocity of the discharge port is equal to flow rate divided by the cross-sectional area of the discharge pipe (velocity = flow/area). The flow rate for the baseline is the rated capacity of the MPCD (i.e., 10 gpm for the gravity coalescer). The area is calculated from the diameter of the discharge pipe. The duration of the release event is based on the size of the OWHT, the rated capacity of any control in place, and the bilgewater generation rate. The volume of bilgewater being processed is based upon Navy practices, which assumes bilgewater processing begins when the OWHT reaches 90 percent capacity (Smith, B., 2001). The duration is calculated as follows:

Duration of Release Event = (0.90 * OWHT Volume) / (Rated MPCD Capacity – Bilgewater Generation Rate)

The time between release events is determined using bilgewater generation rate data and OWHT capacities. Again, for purposes of modeling it is assumed that the entire discharge release/non-release cycle (a release event followed by the time between release events) occurs while the vessel is pierside. The formulas used to determine some of the values in the physical parameters section are presented in Appendix A.

3.1.1.2 Constituent Data, Classical Data, and other Descriptors

Chemical Data

During UNDS Phase I, sampling was conducted aboard one vessel of the CVN 68 Class, USS JOHN C. STENNIS (CVN 74), from 5 March 1997 to 7 March 1997. This sampling episode serves as the primary source of chemical data for this vessel group.

The samples were analyzed by ETS Analytical Services and Pacific Analytical, Inc. The subsequent results were reviewed by the EPA and DoD to determine the quality of the analytical data; however, some sample data were excluded, in the final calculations, as documented in the *Sampling Episode Report - Volume II -USS JOHN C. STENNIS* (Navy, 1998) based upon Sample Control Center (SCC) review. Data quality was considered for all analyses conducted. To ensure data quality after reviewing documented matrix spike failures and process information discrepancies, a confirmation analysis was conducted for pesticides. This confirmation analysis revealed that there were no pesticides present in the reanalyzed samples. As a result, pesticides are not included in bilgewater discharge profiles (Navy and EPA, 2003).

SCC validated data include the constituents present in the waste stream and their concentrations. Sampling was conducted on the OWS influent, which was considered the untreated baseline for

this vessel group. Several methods used for analyses during Phase I are different than those used for Phase II analyses. For example, mercury was analyzed by EPA Method 1631 for Phase I, but for Phase II samples, EPA Method 1620 was used. The primary difference between these methods is that Method 1631 has a lower detection limit than Method 1620. The decision to use Method 1620 in place of Method 1631 was due to the susceptibility of Method 1631 to a variety of interferences stemming from machinery room equipment. After reviewing Phase I analytical data, EPA Method 1620, with the higher detection level, was found to be suitable for Phase II because constituents were found in sufficiently high concentrations that the cost of using more sensitive and expensive techniques was unjustified. The sampling and analytical decisions made for samples collected on the CVN 74 are detailed in the SSAP. Four field samples were taken during each sampling episode from the influent (representing the baseline) to the OWS. For more information see the *Sampling Episode Report Volume II –USS JOHN C. STENNIS (CVN 74)* (Navy, 1998).

Constituent concentrations are represented by the geometric mean of the measured concentrations in the influent samples. See Appendix B for final constituent values.

Field Information

Field information refers to data obtained at the time of sample collection. Field tests that were conducted on the CVN 74 included pH, temperature, salinity, specific conductance, and free and total chlorine. For these field tests, the reported value was determined by calculating an average of all field measurements. Table 3-2 lists the values for each parameter.

| Field Parameters | Values | | |
|----------------------|------------|--|--|
| рН | 6.9 | | |
| Temperature | 16 °C | | |
| Salinity | 6.8 ppt | | |
| Specific Conductance | 8500 μS/cm | | |
| Free Chlorine | 0.13 mg/L | | |
| Total Chlorine | 0.18mg/L | | |

Table 3-2. Field Testing Results for CVN 68 Baseline

Descriptive Information

Descriptive information refers to data collected to facilitate the environmental effects analysis and is presented here to give a more complete description of the discharge. This information included measurements or observations of color, floating materials, settleable materials, colloidal matter, and turbidity. For parameters based on direct observations, the value was reported from these samples. The laboratory reported the samples were cloudy and colorless; this description was used as an observation for turbidity/colloidal matter. Because the laboratory did not note any floating materials, "None specifically observed in samples collected" was used for this parameter. Foam, odor, scum, and total dissolved gases were not measured for the samples collected. Table 3-3, lists the values for the descriptive data.

Table 3-3. Descriptive Discharge Profile for CVN 68 Baseline

| Narrative Parameters | Field Observations |
|----------------------------|---|
| Color | Cloudy, colorless |
| Floating Materials | None specifically observed in samples collected |
| Foam | None specifically observed in samples collected |
| Odor | None specifically observed in samples collected |
| Scum | None specifically observed in samples collected |
| Settleable Materials | None specifically observed in samples collected |
| Total Dissolved Gases | Not measured in samples collected |
| Turbidity/Colloidal Matter | Cloudy, colorless |

3.1.1.3 Discharge Generation Rates for Mass Loading

All CVN Class vessels are stationed in saltwater ports and do not operate in freshwater. Daily generation rates were obtained from previously reported underway surveys (Navy, 1997a and 1995), which assume that in-port generation rates are approximately 25 percent of the underway generation rates. The annual discharge volumes are derived in Table 3-4 by multiplying these reported values by the average number of days that the class spends in port or at sea.

Table 3-4. Annual Generation Volumes for CVN 68 Baseline

| | | Davs | Davs | Days | Daily generation rate per vessel (gal/day) | | | Annual generation rate per class (gal/year) | | | |
|--------|-------------------|------------|-----------------------|----------------------|--|-----------------------|----------------------|---|-----------------------|----------------------|--|
| Class | Number of Vessels | In Port | Underway (0-12 nm) | Underway (12+ nm) | In port | Underway (0-12 nm) | Underway (12+ nm) | In port | Underway (0-12 nm) | Underway (12+ nm) | |
| | | | | | 1.7E+04 | 6.8E+04 | 6.8E+04 | 2.5E+07 | 2.0E+06 | 1.5E+07 | |
| CVN 65 | 1 | 147 | 3 | 215 | 1.7E+04 | 6.8E+04 | 6.8E+04 | 2.5E+06 | 2.0E+05 | 1.5E+06 | |
| Total | 11 | 1 | - | - | 3.4E+04 | 1.4E+05 | 1.4E+05 | 2.8E+07 | 2.2E+06 | 1.7E+07 | |

3.2 PRIMARY TREATMENT

Gravity coalescer represents the currently installed primary treatment MPCD onboard CVN 68 Class vessels. Most ships of the CVN 68 Class currently have two 50gpm OWS that discharge into a common line with a single discharge location. Because only one OWS is normally used within 12 nm, subsequent analyses are based on one of the two 50-gpm systems processing the entire volume of bilgewater. Primary treatment creates two waste streams: the aqueous fraction, which is discharged overboard, and the oil fraction, which is directed to the onboard waste oil holding tank. The characterization of the aqueous fraction is described below. The oil fraction is subject to collection, holding and transfer (CHT), treatment at a properly-permitted facility, applicable Federal, State, and local disposal regulations.

3.2.1 Characterization Data

Characterization data is comprised of physical parameters, chemical data, field data, and descriptive information. Each of these parameters is discussed below. See Section 3.1.1 for identification of possible bilgewater sources.

3.2.1.1 Physical Parameters

The physical parameters used for hydrodynamic modeling of the discharge, as detailed in Section 3.1.1.1, are not affected by the addition of a primary MPCD. Table 3-5 summarizes the parameters used for modeling purposes.

Table 3-5. Discharge Characteristics for CVN 68 Primary Treatment

| Modeling Parameters | Values |
|----------------------------------|-------------------|
| Option Group | Primary Treatment |
| Vertical (ft) | 3.2 |
| Transverse (ft) | 67 |
| Length (ft) | 885 |
| Diameter (in) | 3 |
| Temperature (°C) | 25 |
| Salinity (ppt) | 8.9 |
| Flow (gpm) | 50 |
| Velocity (ft/sec) | 2.3 |
| Duration of Release Event (hr) | 16.6 |
| Time Between Release Events (hr) | 36.8 |

Vertical – Approximate distance from waterline to discharge port (+, above, -, below)

Transverse – Distance from centerline to discharge port (+, port, -, stbd)

Length – Approximate distance from forward perpendicular to discharge port

Diameter – Diameter of discharge port

ppt– parts per thousand

gpm – gallons per minute

ft/sec – feet per second

hr - hour

°C - Degree Celsius

The formulas used to determine some of the values in the physical parameters section are presented in Appendix A.

3.2.1.2 Constituent Data, Classical Data, and Other Descriptors

Chemical Data

During Phase I of UNDS, Sampling was conducted on one CVN 68 Class vessel, USS JOHN C. STENNIS (CVN 74), and serves as the primary source of chemical data for this vessel group. The samples from this ship were taken prior to and following the gravity coalescer. Constituent concentrations are represented as the geometric mean of the measured concentrations in the effluent samples. Some analytical data were excluded, as documented in the Sample Episode Report (SER), based upon SCC review of the data. See Appendix B for final constituent values.

Field Information

Field information refers to data obtained at the time of sample collection. Field tests conducted on the gravity coalescer samples from the CVN 74 included pH, temperature, salinity, specific conductance, and free and total chlorine. For these field tests, the reported value was determined

by calculating an average of all field measurements. Table 3-6 lists the values for each parameter.

Table 3-6. Field Testing Results for CVN 68 Primary Treatment

| Field Parameters | Values |
|----------------------|-------------|
| рН | 7.3 |
| Temperature | 16 °C |
| Salinity | 11 ppt |
| Specific Conductance | 11000 μS/cm |
| Free Chlorine | 0.1 mg/L |
| Total Chlorine | 0.1 mg/L |

Descriptive Information

Descriptive observations and tests were conducted on the MPCD gravity coalescer effluent samples from the CVN 74. This information included observations or measurements of color, floating material, odor, settleable materials, turbidity and colloidal matter. For parameters based on direct observations (color and odor), the reported determinations were based upon these. For the parameters based on measurements, an average result was used as the reported value except for the total dissolved gases parameter. The laboratory reported the samples were cloudy and colorless; this description was used as an observation for turbidity/colloidal matter. Because the laboratory did not note any floating materials, "not observed" was used for this parameter. Foam, odor, scum, taste, and total dissolved gases were not measured for the samples collected. The values for these descriptive parameters is listed as "not measured". Table 3-7 lists the values for all descriptive parameters.

Table 3-7. Descriptive Discharge Profile for CVN 68 Primary Treatment

| Narrative Parameters | Field Observations | | |
|----------------------------|---|--|--|
| Color | Cloudy-Opaque/ Colorless | | |
| Floating Materials | None specifically observed in samples collected | | |
| Foam | None specifically observed in samples collected | | |
| Odor | None specifically observed in samples collected | | |
| Scum | None specifically observed in samples collected | | |
| Settleable Materials | None specifically observed in samples collected | | |
| Total Dissolved Gases | Not measured in samples collected | | |
| Turbidity/Colloidal Matter | Opaque-Cloudy/No | | |

3.2.1.3 Discharge Generation Rates for Mass Loading

The use of a primary treatment MPCD does not affect the generation rate of bilgewater; therefore, the baseline generation and annual volume data are used for the annual discharge volume for this MPCD treatment system. It is assumed that the volume change due to the removal of oil by the treatment device is negligible. See Table 3-4, Section 3.1.1.3, for the baseline generation volumes.

3.3 PRIMARY TREATMENT PLUS FILTER MEDIA

This MPCD option involves treatment with a primary treatment MPCD followed by a secondary treatment through filter media. Primary treatment plus filter media creates two waste streams: the aqueous fraction, which is discharged overboard, and the oil fraction, which is directed to the onboard waste oil holding tank. After initial treatment by the OWS, the aqueous waste stream is either re-directed back to the OWHT for reprocessing or sent to the polisher (i.e., filter media) system. This is controlled by monitoring the waste stream oil concentration with an oil content monitor (OCM). For concentrations greater than 200 ppm, the waste stream is returned to the OWHT for re-circulation through the OWS, whereas for oil concentrations less than 200 ppm, the waste stream is sent on to the filter media system (Navy, 2000c). The filter media discharge is also monitored. Effluent with oil concentration less than 15 ppm, is released overboard while wastewater with a greater than 15 ppm, it is returned to the OWHT for additional processing (Navy, 2000c). The oil fraction is subject to CHT treatment at a properly-permitted facility and applicable Federal, State, and local disposal regulations.

The characterization of the aqueous fraction is described below.

3.3.1 Characterization Data

Characterization data are comprised of physical parameters, chemical data, field data, and descriptive information. Each of these parameters is discussed below. See Section 3.1.1 for identification of possible bilgewater sources.

3.3.1.1 Physical Parameters

The physical parameters used for hydrodynamic modeling purposes, as detailed in Section 3.1.1.1, are not affected by the addition of primary and secondary MPCDs. Table 3-8 summarizes the parameters identified for modeling purposes.

Table 3-8. Discharge Characteristics for CVN 68 Primary Treatment plus Filter Media

| Modeling Parameters | Values |
|----------------------------------|-------------------------------------|
| Option Group | Primary Treatment plus filter media |
| Vertical (ft) | 3.2 |
| Transverse (ft) | 67 |
| Length (ft) | 885 |
| Diameter (in) | 3 |
| Temperature (°C) | 25 |
| Salinity (ppt) | 8.9 |
| Flow (gpm) | 50 |
| Velocity (ft/sec) | 2.3 |
| Duration of Release Event (hr) | 16.6 |
| Time Between Release Events (hr) | 36.8 |

Vertical – Approximate distance from waterline to discharge port (+, above, -, below)

Transverse – Distance from centerline to discharge port (+, port, -, stbd)

Length – Approximate distance from forward perpendicular to discharge port

Diameter – Diameter of discharge port

ppt – parts per thousand

gpm – gallons per minute

ft/sec - feet per second

hr - hour

°C - Degree Celsius

The formulas used to determine some of the values in the physical parameters section are presented in Appendix A.

3.3.1.2 Constituent Data, Classical Data, and Other Descriptors

Chemical Data

Using bilgewater effluent data, the Naval Surface Warfare Center Carderock Division (NSWCCD) evaluated the treatment capabilities for filter media. The filter media MPCD is comprised of an oleophilic blend of granular polymer and carbon media. Although the polymer was designed to remove oil by entrainment and sorption, the carbon media will reduce the concentrations of semi-volatile organic constituents, especially polynuclear aromatic hydrocarbons (PAHs) (Putnam and Singerman, 2001). Table 3-9 contains the treatment capabilities detailed within the NSWCCD report for filter media and the necessary calculations on the primary treatment MPCD constituents.

Table 3-9. Treatment Capabilities of Filter Media (Putnam and Singerman, 2001)

| Analyte Class | Empirical Formulas for Constituent Concentrations |
|------------------------|---|
| Classical | Ammonia as Nitrogen = C_i Nitrite/Nitrate = $0.6C_i$ Oil & Grease (HEM) = $0.3C_i$ TPH (SGT-HEM) = $0.3C_i$ Total Sulfide = $0.2C_i$ TSS = $0.43C_i$ |
| Total Metals | $\begin{aligned} & \text{Copper} = 0.5 \text{M}_t \\ & \text{Iron} = 0.4 \text{M}_t \\ & \text{Nickel} = 0.75 \text{M}_t \\ & \text{Zinc} = 0.6 \text{M}_t \\ & \text{All others} = \text{M}_t \end{aligned}$ |
| Semi-volatile Organics | $=0.4C_{i}$ |
| Volatile Organics | Chlorobenzene = 0.20C _i M+p-Xylene = 0.20C _i |

C_i is the concentration of the constituent in the input stream.

Applying these treatment capabilities of filter media to the results for the constituents of the OWS effluent produces the constituent concentrations expected by incorporating filter media (Table 3-10). See Appendix B for complete list of constituent values.

Table 3-10. Calculated Constituent Concentrations for CVN 68 Primary Treatment Plus Filter Media

| Constituent | CAS Number | Primary Treatment | Data Qualifier | Estimated Concentrations Primary Treatment plus Filter Media | Data Qualifier |
|---|---------------|----------------------|-------------------|---|-------------------|
| Classicals (mg/L) | | | , | | |
| Ammonia as Nitrogen | 7664417 | 1.30E-01 | | 1.30E-01 | |
| Biochemical Oxygen Demand (BOD) | C003 | 1.00E+01 | | 1.00E+01 | |
| Chemical Oxygen Demand (COD) | C004 | 1.80E+02 | | 1.80E+02 | |
| Nitrate/Nitrite | C005 | 2.70E-01 | | 1.60E-01 | |
| Oil and Grease (as HEM) | C036 | 2.30E+01 | | 6.80E+00 | |
| SGT-HEM | C037 | 9.40E+00 | | 5.00E+00 | U |
| Total Kjeldahl Nitrogen (TKN) | C021 | 1.50E+00 | | 1.50E+00 | |
| Total Phosphorous | 14265442 | 1.80E+00 | | 1.80E+00 | |
| Total Recoverable Oil & Grease (as HEM) | C007 | 4.40E+01 | | 1.30E+01 | |
| Total Sulfide | 18496258 | 5.00E+00 | | 1.00E+00 | |
| Total Suspended Solids (TSS) | C009 | 4.20E+01 | | 1.80E+01 | |
| Semivolatile Organics (ug/L) | | | | | |
| 2,4-Dimethylphenol | 105679 | 1.00E+01 | U | 1.00E+01 | U |
| 2-Chloronapthalene | 91587 | 1.00E+01 | U | 1.00E+01 | U |
| 2-Methylnapthalene | 91576 | 1.00E+01 | U | 1.00E+01 | U |
| Acenapthene | 83329 | 1.00E+01 | U | 1.00E+01 | U |
| Bis-(2-ethylhexyl) Phthalate | 117817 | 1.00E+01 | U | 1.00E+01 | U |
| Dibenzofuran | 132649 | 1.00E+01 | U | 1.00E+01 | U |

 $[\]dot{M_t}$ is the total concentration of the metal in the input stream.

| Constituent | CAS Number | Primary Treatment | Data Qualifier | Estimated Concentrations Primary Treatment plus Filter Media | Data Qualifier |
|--------------------------|---------------|----------------------|-------------------|---|-------------------|
| Fluorene | 86737 | 1.00E+01 | U | 1.00E+01 | U |
| N,N-Dimethylformamide | 68122 | 5.80E+01 | | 2.30E+01 | |
| Naphthalene | 91203 | 1.00E+01 | U | 1.00E+01 | U |
| Phenanthrene | 85018 | 1.00E+01 | U | 1.00E+01 | U |
| Volatile Organics (ug/L) | | | | | |
| Chlorobenzene | 108907 | 1.00E+01 | U | 1.00E+01 | U |
| o+p-Xylene | 136777612 | 1.10E+01 | | 1.00E+01 | U |
| Toluene | 108883 | 1.00E+01 | U | 1.00E+01 | U |
| Total Metals (ug/L) | | | , | | |
| Aluminum | 7429905 | 1.50E+02 | | 1.50E+02 | |
| Antimony | 7440360 | 6.80E+00 | | 6.80E+00 | |
| Arsenic | 7440382 | 1.00E+01 | | 1.00E+01 | U |
| Barium | 7440393 | 3.70E+01 | | 3.70E+01 | |
| Boron | 7440428 | 1.50E+03 | | 1.50E+03 | |
| Cadmium | 7440439 | 5.10E+00 | | 5.10E+00 | |
| Calcium | 7440702 | 1.30E+05 | | 1.30E+05 | |
| Copper | 7440508 | 3.40E+02 | | 1.70E+02 | |
| Iron | 7439896 | 4.70E+02 | | 1.90E+02 | |
| Lead | 7439921 | 4.60E+01 | U | 4.60E+01 | U |
| Magnesium | 7439954 | 4.30E+05 | | 4.30E+05 | |
| Manganese | 7439965 | 3.00E+01 | | 3.00E+01 | |
| Mercury | 7439976 | 5.20E-02 | | 5.20E-02 | |
| Molybdenum | 7439987 | 1.30E+01 | | 2.00E+01 | U |
| Nickel | 7440020 | 1.70E+02 | | 1.30E+02 | |
| Selenium | 7782492 | 2.00E+01 | U | 2.00E+01 | U |
| Silver | 7440224 | 5.00E+00 | U | 5.00E+00 | U |
| Sodium | 7440235 | 3.60E+06 | | 3.60E+06 | |
| Thallium | 7440280 | 1.00E+01 | U | 1.00E+01 | U |
| Titanium | 7440326 | 6.30E+00 | | 6.30E+00 | |
| Zinc | 7440666 | 8.90E+02 | | 5.30E+02 | |

U - Not detected in waste stream

For additional information on the capabilities of filter media, NSWCCD conducted field testing of two filter media systems. The systems were on USS GONZALES (DDG 66) and USS ROSS (DDG 71). The testing was undertaken to evaluate the performance of filter media and its subsequent ability to improve the quality of the water discharged from the OWS.

Testing showed that although the filter media functioned to remove oil, it was not consistently effective at achieving oil concentrations of less than 15 ppm. In the more favorable of two cases, the oil concentration was less than 15 ppm in only 32 percent of the effluent samples taken. For the second test the filter media system was even less effective at obtaining concentrations below

15 ppm. Both tests demonstrated that the percentage of oil removed by the filter media system was closely related to the OWS influent oil concentration (specifically, the higher the levels of influent particulate, the less efficient the removal process) (Navy, 2001e).

Although the findings did not support filter media achieving the less than 15 ppm oil concentration sought, it was concluded that the filter media system did reduce the discharged oil concentrations below those of the gravity coalescer system alone.

Field Information

Field tests conducted on CVN 74 included pH, temperature, salinity, specific conductance, and free and total chlorine (Table 3-11). Based on the observed relationship between the gravity coalescer and gravity coalescer plus a secondary MPCD for samples taken for the DDG 51 vessel group, the addition of a secondary MPCD is not expected to change the values for the field parameters. As a result, the reported values for the gravity coalescer samples were used to represent the primary treatment plus filter media values for the CVN 68 vessel group.

| Table 3-11. Field | lesting Results for | CVN 68 Primary | Treatment Plus | Filter Media |
|-------------------|---------------------|----------------|----------------|--------------|
| | | | | |

| Field Parameters | Values |
|----------------------|------------|
| рН | 7.3 |
| Temperature | 15 °C |
| Salinity | 11 ppt |
| Specific Conductance | 8500 μS/cm |
| Free Chlorine | 0.1 mg/L |
| Total Chlorine | 0.1 mg/L |

Descriptive Information

Descriptive tests were conducted on the MPCD gravity coalescer effluent samples from CVN 74. This information included observations or measurements of color, floating material, odor, settleable materials, and turbidity/colloidal matter. The data for these parameters were not specifically observed for the CVN 68 vessel group for a gravity coalescer plus filter media MPCD option so the descriptive test could not be captured for this MPCD option. However, based on a review of the filter media results for the DDG 51 vessel group, the change in color from primary treatment to primary treatment plus filter media went from black to dark gray. For the CVN 68 Vessel group the primary treatment effluent samples were recorded as opaque/cloudy, colorless. Based on a similar degree of change it is assumed that color will be reduced but not eliminated.

A similar degree of change was extrapolated for all narrative parameters for primary treatment plus filter media. However, no other parameters were specifically observed for this MPCD option for the CVN 68 Vessel group.

3.3.1.3 Discharge Generation Rates for Mass Loading

The use of a primary and secondary MPCD does not affect the generation rate of bilgewater; therefore, the baseline generation and annual volume data are used for the annual discharge volume for this MPCD treatment. It is assumed that the volume change due to the removal of oil by both treatment devices is negligible. See Table 3-4, Section 3.1.1.3, for the baseline generation volumes.

3.4 PRIMARY TREATMENT PLUS MEMBRANE FILTRATION

This MPCD option involves the wastestream being processed by a primary treatment MPCD followed by the secondary treatment of membrane filtration. Primary treatment plus membrane filtration creates two waste streams: the aqueous fraction, which is discharged overboard, and the oil fraction, which is directed to the onboard waste oil holding tank. The characterization of the aqueous fraction is described below. The oil fraction is subject to CHT, treatment at a permitted facility, and applicable Federal, State, and local disposal regulations.

3.4.1 Characterization Data

Characterization data is comprised of physical parameters, chemical data, field data, and descriptive information. Each of these parameters are discussed below. See Section 3.1.1 for identification of possible bilgewater sources.

3.4.1.1 Physical Parameters

The physical parameters used for hydrodynamic modeling purposes, as detailed in Section 3.1.1.1, are not affected by the addition of primary and secondary MPCDs. Table 3-12 summarizes the parameters identified for modeling purposes.

Table 3-12. Discharge Characteristics for CVN 68 Primary Treatment plus Membrane Filtration

| Modeling Parameters | Values | | | |
|----------------------------------|--|--|--|--|
| Option Group | Primary Treatment plus membrane filtration | | | |
| Vertical (ft) | 3.2 | | | |
| Transverse (ft) | 67 | | | |
| Length (ft) | 885 | | | |
| Diameter (in) | 3 | | | |
| Temperature (°C) | 25 | | | |
| Salinity (ppt) | 8.9 | | | |
| Flow (gpm) | 50 | | | |
| Velocity (ft/sec) | 2.3 | | | |
| Duration of Release Event (hr) | 16.6 | | | |
| Time Between Release Events (hr) | 36.8 | | | |

Vertical – Approximate distance from waterline to discharge port (+, above, -, below)

Transverse – Distance from centerline to discharge port (+, port, -, stbd)

Length – Approximate distance from forward perpendicular to discharge port

Diameter - Diameter of discharge port

ppt – parts per thousand

gpm - gallons per minute

ft/ sec - feet per second

hr - hour

°C - Degree Celsius

The calculations used to determine some of the values in the physical parameters section are presented in Appendix A.

3.4.1.2 Constituent Data, Classical Data, and Other Descriptors

Chemical Data

Using bilgewater effluent data, the NSWCCD evaluated the treatment capabilities for a ceramic ultrafiltration membrane system. Ceramic ultrafiltration membrane (i.e., membrane filtration) systems are hydrophilic with an amorphous silica separation layer atop a highly porous magnesium aluminosilicate substrate (Tompkins and Owsenek, 1996). Within these systems, bilgewater is recirculated through the membrane module at high velocities. The recirculation effectively increases the time for equilibrium, and the high flow velocities create turbulence and agitation that facilitate equilibration. Recirculation conditions favor the transport of materials between the oil and water phases, particularly from the water to the oil. Processing of inorganic solutes and organic liquids resulted in reduced membrane performance. These constituents were transported through the membrane regardless of whether equilibrium favors the oil phase. Also, in cases where there was a high detergent concentration there was a temporary but significant decrease in membrane flux.

NSWCCD, in a contractor analysis report by Native American Consultants, Inc., (Putnam and Singerman, 2001), developed the theory that the transport of pesticides, herbicides, volatile organic material, and semivolatile organic material constituents through a ceramic ultrafiltration membrane (i.e., membrane filtration) is related to the water solubility of the constituents, due to

the phase separation achieved by the membrane. Technical data from USS CARNEY (DDG 64) (Rose, Pehrsson, et al., 1997) indicated that most of the constituents that had water solubilities greater than 30 mg/L, passed through the membrane, while most of the constituents with water solubility of less than 1 mg/L did not pass through the membrane.

Table 3-13 details the membrane filtration treatment capabilities.

Table 3-13. Treatment Capabilities of Membrane Filtration (Putnam and Singerman, 2001)

| Analyte Class | Empirical Formulas for Constituent Concentrations |
|-----------------------|--|
| Classical | Ammonia as Nitrogen = C_i Nitrite/Nitrate = C_i Oil & Grease (HEM) = 8.5 mg/L, C_i ; whichever is less TPH (SGT-HEM) = 3.5 mg/L, C_i ; whichever is less Total Sulfide = 0.15 C_i TSS = 0.3 C_i |
| Total Metals | $\begin{aligned} &M_t \leq M_d, = M_d \\ &\text{Otherwise,} \\ &= 0.2 \ (M_t - M_d) + M_d \end{aligned}$ |
| Semivolatile Organics | $S_w \le 0.1 \text{ mg/L}, = 0$ $S_w \ge 30 \text{ mg/L}, = C_i$ Otherwise, $= C_i(0.03344S_w - 0.003344)$ |
| Volatile Organics | $S_w \le 0.1 \text{ mg/L}, = 0$ $S_w \ge 30 \text{ mg/L}, = C_i$ Otherwise, $= C_i(0.03344S_w - 0.003344)$ |

 C_{i} is the concentration of the constituent in the input stream.

Applying these treatment capabilities to the results for the gravity coalescer discharge produces the expected constituent concentrations for the primary treatment followed by a secondary MPCD option of membrane filtration (Table 3-14). See Appendix B for complete list of final constituent values.

Table 3-14. Calculated Constituent Concentrations for CVN 68 Primary Treatment Plus Membrane Filtration

| Constituent | CAS Number | Primary Treatment | Data Qualifier | Estimated Concentration Primary Treatment plus Membrane Filtration | Data Qualifier |
|---------------------------------|---------------|----------------------|-------------------|--|-------------------|
| Classicals (mg/L) | | | | | |
| Ammonia as Nitrogen | 7664417 | 1.30E-01 | | 1.30E-01 | |
| Biochemical Oxygen Demand (BOD) | C003 | 1.00E+01 | | 1.00E+01 | |
| Chemical Oxygen Demand (COD) | C004 | 1.80E+02 | | 1.80E+02 | |
| Nitrate/Nitrite | C005 | 2.70E-01 | | 2.70E-01 | |
| Oil and Grease (as HEM) | C036 | 2.30E+01 | | 8.50E+00 | |
| SGT-HEM | C037 | 9.40E+00 | | 5.00E+00 | U |
| Total Kjeldahl Nitrogen (TKN) | C021 | 1.50E+00 | | 1.50E+00 | |

 M_{t} is the total concentration of the metal in the input stream.

M_d is the concentration of the dissolved metal in the input stream.

S_w is the water solubility of the constituent in mg/L.

| Constituent | CAS Number | Primary Treatment | Data Qualifier | Estimated Concentration Primary Treatment plus Membrane Filtration | Data Qualifier |
|---|---------------|----------------------|-------------------|--|-------------------|
| Total Phosphorous | 14265442 | 1.80E+00 | | 1.80E+00 | |
| Total Recoverable Oil & Grease (as HEM) | C007 | 4.40E+01 | | 8.50E+00 | |
| Total Sulfide | 18496258 | 5.00E+00 | | 1.00E+00 | U |
| Total Suspended Solids (TSS) | C009 | 4.20E+01 | | 1.27E+01 | |
| Semivolatile Organics (ug/L) | | | | | |
| 2,4-Dimethylphenol | 105679 | 1.00E+01 | U | 1.00E+01 | U |
| 2-Chloronapthalene | 91587 | 1.00E+01 | U | 1.00E+01 | U |
| 2-Methylnapthalene | 91576 | 1.00E+01 | U | 1.00E+01 | U |
| Acenapthene | 83329 | 1.00E+01 | U | 1.00E+01 | U |
| Bis-(2-ethylhexyl) Phthalate | 117817 | 1.00E+01 | U | 1.00E+01 | U |
| Dibenzofuran | 132649 | 1.00E+01 | U | 1.00E+01 | U |
| Fluorene | 86737 | 1.00E+01 | U | 1.00E+01 | U |
| N,N-Dimethylformamide | 68122 | 5.80E+01 | | 1.00E+01 | U |
| Naphthalene | 91203 | 1.00E+01 | U | 1.00E+01 | U |
| Phenanthrene | 85018 | 1.00E+01 | U | 1.00E+01 | U |
| Volatile Organics (ug/L) | | | | | |
| Chlorobenzene | 108907 | 1.00E+01 | U | 1.00E+01 | U |
| o+p-Xylene | 136777612 | 1.10E+01 | | 1.10E+01 | |
| Toluene | 108883 | 1.00E+01 | U | 1.00E+01 | |
| Total Metals (ug/L) | | | | | |
| Aluminum | 7429905 | 1.50E+02 | | 4.80E+01 | U |
| Antimony | 7440360 | 6.80E+00 | | 2.00E+00 | U |
| Arsenic | 7440382 | 1.00E+01 | | 1.00E+01 | U |
| Barium | 7440393 | 3.70E+01 | | 3.50E+01 | |
| Boron | 7440428 | 1.50E+03 | | 1.60E+03 | |
| Cadmium | 7440439 | 5.10E+00 | | 5.00E+00 | U |
| Calcium | 7440702 | 1.30E+05 | | 1.40E+04 | |
| Copper | 7440508 | 3.40E+02 | | 2.00E+02 | |
| Iron | 7439896 | 4.70E+02 | | 9.40E+01 | |
| Lead | 7439921 | 4.60E+01 | U | 4.60E+01 | U |
| Magnesium | 7439954 | 4.30E+05 | | 4.00E+05 | |
| Manganese | 7439965 | 3.00E+01 | | 2.70E+01 | |
| Mercury | 7439976 | 5.2E-02 | | 5.2E-02 | |
| Molybdenum | 7439987 | 1.30E+01 | | 2.10E+01 | |
| Nickel | 7440020 | 1.70E+02 | | 1.80E+02 | |
| Selenium | 7782492 | 2.00E+01 | U | 2.00E+01 | U |
| Silver | 7440224 | 5.00E+00 | U | 5.00E+00 | U |
| Sodium | 7440235 | 3.60E+06 | | 3.60E+06 | |
| Thallium | 7440280 | 1.00E+01 | U | 1.00E+01 | U |
| Titanium | 7440326 | 6.30E+00 | | 5.00E+00 | U |

| Constituent | CAS Number | Primary Treatment | Data Qualifier | Estimated Concentration Primary Treatment plus Membrane Filtration | Data Qualifier |
|-------------|---------------|----------------------|-------------------|--|-------------------|
| Zinc | 7440666 | 8.90E+02 | | 8.61E+02 | |

U - Not detected in wastestream

To further evaluate the treatment capabilities of membrane filtration systems, a study was undertaken by NSWCCD to determine if the chemical constituents found in bilgewater could potentially damage the ceramic membrane systems, thus reducing their ability to process oily waste effectively (Navy, 1996). To facilitate this study, 26 mixtures and compounds with the potential to be found in bilgewater were processed. This testing was intended to determine the level of fouling following the treatment of these constituents and their impact on the processing ability of the membrane filtration system.

The evaluation of 11 different types of constituents and one pH analysis were conducted on a membrane filtration system. The goal of these analyses was to determine the ability of membrane filtration system to consistently produce an effluent that would conform to local and worldwide environmental standards regardless of influent concentrations. Test results indicated that membrane filtration is capable of conforming to these standards while operating over a wide range of pHs and is resistant to chemical attack. High concentrations of inorganic and organic compounds (i.e., saline solutions, paints and primers, oxidizers, aqueous film-forming foam, or treatment preparations) led to reduced membrane performance. However, despite these minor reductions in processing capacity, most membranes recovered significantly when flushed with water for 15 minutes (Navy, 1996).

Field Information

Field tests conducted on CVN68 included pH, temperature, salinity, specific conductance, and free and total chlorine (Table 3-15). Based on the observed relationship between the gravity coalescer and gravity coalescer plus a secondary MPCD for samples taken for the DDG 51 vessel group, the addition of a secondary MPCD is not expected to change the values for the field parameters. As a result, the reported values for the gravity coalescer samples were used to represent the primary treatment plus membrane filtration values for the CVN 68 vessel group.

Table 3-15. Field Testing Results for CVN 68 Primary Treatment Plus Membrane Filtration

| Field Parameters | Values | | |
|----------------------|------------|--|--|
| pH | 7.3 | | |
| Temperature | 15 °C | | |
| Salinity | 11 ppt | | |
| Specific Conductance | 8500 μS/cm | | |
| Free Chlorine | 0.1 mg/L | | |
| Total Chlorine | 0.1 mg/L | | |

Descriptive Information

Descriptive tests were conducted on the MPCD gravity coalescer effluent samples from CVN 74. This information included observations or measurements of color, floating material, odor, settleable materials, and turbidity/colloidal matter. The data for these parameters were not specifically observed on the CVN 74 for a gravity coalescer plus membrane filtration so the descriptive test could not be captured for this MPCD option. However, based on a review of the membrane filtration results for the LSD 41 vessel group, there was no change in color observed from primary treatment to primary treatment plus membrane filtration. Consequently, it is assumed there is no color change from primary treatment to primary treatment plus membrane filtration for the CVN 68 vessel group.

A similar degree of change was extrapolated for all narrative parameters for primary treatment plus membrane filtration. However, no other parameters were specifically observed for this MPCD option for the CVN 68 Vessel group.

3.4.1.3 Discharge Generation Rates for Mass Loading

The use of primary and secondary MPCDs does not affect the generation rate of bilgewater; therefore, the baseline generation and annual volume data are used for the annual discharge volume for this MPCD treatment system. It is assumed that the volume change due to the removal of oil by treatment device is negligible. See Table 3-4, Section 3.1.1.3, for the baseline generation volumes.

3.5 COLLECTION, HOLDING, AND TRANSFER WITHIN 12NM

CHT is the onboard collection, containment, and subsequent transfer of bilgewater to shore facilities or ship waste offload barges. CHT does not involve any treatment of raw bilgewater on board the generating vessel. CHT may require the installation of some shipboard equipment, such as piping or tanks, to provide additional holding capacity. This MPCD option results in no (zero) liquid discharge to surrounding waters within 12 nm.

3.5.1 Characterization Data

Characterization data are comprised of physical parameters, chemical data, field data, and descriptive information. Each of these parameters is discussed below. See Section 3.1.1 for identification of bilgewater sources. However, because this MPCD option results in no (zero) direct liquid discharge to surrounding waters within 12 nm, there is no characterization data to address.

3.5.1.1 Physical Parameters

This MPCD option results in no (zero) direct liquid discharge to surrounding waters within 12 nm, therefore there are no discharge characteristics to consider.

3.5.1.2 Constituent Data, Classical Data, and Other Descriptors

Chemical Data

Because a waste stream is not directly discharged to surrounding waters within 12 nm for this MPCD option, there are no constituents to consider.

Field Data

Because a waste stream is not directly discharged to surrounding waters within 12 nm for this MPCD option, there are no field data to consider.

Descriptive Information

Because a waste stream is not directly discharged to surrounding waters within 12 nm for this MPCD option, there is no descriptive information to consider.

3.5.1.3 Discharge Generation Rates for Mass Loading

Collection, holding, and transfer results in no direct liquid discharge to surrounding waters within 12 nm. Therefore, the annual discharge volume is zero.

3.6 UNCERTAINTY AND DATA QUALITY FOR CVN 68 DISCHARGE

The sources and levels of uncertainty in bilgewater characterization data vary by discharge parameter. This subsection describes the uncertainty associated with physical parameters; constituent data, classical data and other descriptors; and discharge generation rates.

3.6.1 Physical Parameters Uncertainty and Data Quality for CVN 68 Discharge

Schematic Data

The information provided for the physical parameters of CVN 68 baseline discharge is based on process knowledge and the vessel specifications of the representative vessel. Certain physical parameter values, including representative vessel length, discharge port diameter, and distance from centerline to discharge port (transverse), used in this report are taken directly from vessel schematics. These parametric values do not vary among vessels in the class. Certain other parameters vary with load conditions. These condition specific parameters include: approximate distance from waterline to discharge port (vertical), approximate distance from forward perpendicular to discharge port (length), and discharge method. The discharge was assumed to occur under full load conditions to facilitate a comparison of baseline and MPCD option performance. This assumption is supported by Armed Forces expert knowledge of ship status, which indicated that when vessels are pierside they typically are loaded for deployment.

Modeling Data

One use of discharge characterization information is to provide input data for hydrodynamic modeling of a discharge plume within a mixing zone. Modeling is performed to determine plume dilution factors at the edge of a mixing zone. Modeling calculations involve various

parameters that include discharge temperature, density, and vessel attributes related to bilgewater discharge, such as the distance from the discharge port to the waterline. The bilgewater temperature was assumed to be equal to ambient water temperature for modeling purposes. Bilgewater is stored in OWHTs in direct contact with the hull, resulting in temperature equilibration. The bilgewater data for salinity was taken from UNDS sampling data. Uncertainty related to sampling is discussed in Section 3.6.2 and applies to the salinity data.

As stated in Section 3.1.1.1, the discharge flow rate used to characterize the discharge is based on the rated capacity of the processor as reported by the manufacturer. The duration of, and time between, release events are closely related and are dependent on the volume of the OWHT. The volume of the OWHT at processing onset determines the duration of the release event. Likewise, the time between release events is related to the capacity of the OWHT and the bilgewater generation rate. A simplifying assumption, that the release of bilgewater discharge occurs when the OWHT reaches 90 percent of capacity, was made based on knowledge derived from equipment experts.

3.6.2 Constituent Data, Classical Data, and Other Descriptors Uncertainty and Data Quality for CVN 68 Discharge

Sampling was conducted aboard the CVN 74 according to the Specified Sampling Analysis Plan (SSAP) (Navy, 1998). Deviations in sampling practices, analytic testing, laboratory equipment, processing equipment, and specimen handling exist and may affect the results. For more information on the sampling plan, see the SSAP for CVN 74.

During the sampling episodes, a number of deviations from the sampling plan were noted in the SER.

- The SSAP called for 5 grab samples to be collected from the influent to the OWS. However, the flow rate for the sampling port was too low to collect individual grab samples. Due to this unforeseen circumstance, the sampling team decided that a composite volume sample would suitably represent the discharge because it captures more volume over a broader period of time, rather than a grab sample that would only represent an instantaneous slug of bilgewater. For this reason, the sampling plans for the other sampled vessels were also adjusted to incorporate composite sampling. However, due to the nature of the analytes being tested (e.g., volatile organic compounds can not be stored in the larger composite container because of the need to minimize head space in the sample bottle), certain samples were still collected as grab rather than composite samples.
- Another deviation that occurred was that only four samples were collected instead of the
 originally planned five samples for pesticides, hydrazine, and cyanide due to a
 malfunctioning vacuum pump. However, for the purposes of our analysis, it does not
 significantly affect the usefulness of the data.

The SER also details issues identified during the sample analysis, including the SCCs review of the analytical data. The reports also contain further details regarding any additional data qualifiers for specific constituents for the samples. A complete description of how qualified data were used in the UNDS program can be found in Section 3.1.1.2.

CVN 74 sample data were used to characterize this vessel group. As described in the *Vessel Grouping Representative Vessel Selection for Surface Vessel Bilgewater/Oil Water Separator Discharge* (Navy and EPA, 2001a), although subsequent decision making resulted in the selection of CVN68 to represent this vessel group, process knowledge indicates that there should be no significant differences in bilgewater composition between vessels of the same class.

Descriptive information (e.g., color and odor) was not recorded during sample collection activities for the CVN 74. The final determinations for these parameters were based on the laboratory records. All descriptive data collected for the CVN were subsequently reviewed by Navy ship systems experts.

3.6.3 Discharge Generation Uncertainty and Data Quality for CVN 68 Discharge

Bilgewater generation rates for nuclear powered aircraft carriers (CVN 68 and CVN 65 classes) used in this report to characterize the discharge are estimated based on process knowledge and previously reported values. The UNDS Phase I Surface Vessel Bilgewater/OWS Nature of Discharge Report (NOD) estimates that the average in-port generation rate for a CVN 68 Class Vessel is estimated at approximately 3,000 gal/day (EPA and DoD, 1999). This estimate was based on a calculated average of six OWS processing events that occurred during a 30-day period. The Navy's David Taylor Research Center estimated that in-port generation rates are 25 percent of the generation underway (Navy, 1997b). Therefore, these two reports suggest an underway generation rate of 12,000 gal/day. However, a Navy report (Navy, 1997a) presented values based on performance data of 17,000 gal/day in port and 68,000 gal/day underway. These differences in generation rates reflect the uncertainty associated with these values. For mass loading calculations and to ensure that potential MPCDs would be capable of treating the discharge, the higher values presented in the 1995 Navy report are used for bilgewater generation rates.